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HEIGHT-GAIN TESTS IN THE TROPOSPHERE

R.R.D.E.

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Air Ministry,
Great Baddow Research Station,
Nr. Chelmsford,
Essex.

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HEIGHT-GAIN TESTS IN THE TROPOSPHERE.

44/3959

Introduction.

An urgent need for prediction of ranges for V.H.F. navigational aids has been expressed by Operational Commands and an intensive research into the prediction of the meteorological conditions, upon which the range of V.H.F. waves so much depends, is being carried out.

The meteorological conditions affect the propagation in so far as they control the variation of the refractive index of the atmosphere with height above ground.

One way in which the refractive index law affects the propagation is in the nature of the height-gain relations at any given distance beyond the horizon.

It is well known that the variation of field strength with height above ground can be greatly modified when there is marked anomalous propagation associated with the formation of a sufficiently tall duct. A direct measurement of the height-gain relationship should therefore give an immediate indication of the existence of abnormal conditions, when the usual increase of field strength with height typical of pure diffraction would be modified. From the nature and degree of the modification it should be possible to assess the refractive index law and its effect on the range of V.H.F. signals received at any given height.

The height-gain relationship should therefore provide a direct and useful indication of propagation conditions.

Mr. Eckersley considered that regular aircraft flights could be made to measure the change in field strength with height at one or more distances below the horizon from a fixed transmitter, analogous to the regular flights now made to obtain meteorological data. Permission was granted by the Air Ministry for some initial experimental flights to be undertaken by 192 Squadron in order to explore the feasibility of the method and the possibility of interpreting the results in relation to range predictions.

This report will deal only with the practical work involved, the conditions under which the measurements were made and the tabulation of the data obtained.

A further report will be made by the Eckersley Group dealing with the analysis and interpretation of the data obtained.

Six experimental flights, under the direction of Mr. Eckersley, were made between January and April of this year, using a frequency of 200 Mc/s.

Equipment.

(a) Receiver.

A modified Hallicrafter S27 CA was used for all these test flights.

The major modification to be made was the insertion of a suitable signal strength measuring device.

A piston type attenuator was inserted in series with the aerial feeder. The particular attenuator available had been designed for 75 ohms

and was therefore suited to one of the standard flexible concentric cables used on aircraft.

As it was hoped to measure field strength variations of the order of 80 decibels it was obviously necessary to pay great attention to the screening of the receiver.

The S.27.CA was therefore taken out of its standard box and put in a 16 S.W.G. brass box with ventilation vents of close mesh brass gauze.

The aerial input to the receiver was modified to an unbalanced circuit by means of a standard Air Ministry socket, the earth portion of the socket being directly connected to the receiver chassis.

The attenuator was fitted on a sloping panel on top of the receiver.

The preliminary laboratory tests showed that the attenuator introduced an insertion loss of 25 dBs. between aerial and receiver input.

In order to reduce this loss to a reasonable value the two electrodes of the piston were arranged to touch in the lowest attenuation position giving an insertion loss of 7 decibels which was considered reasonable; in consequence linear movement of the attenuator dial was sacrificed. To make the lower values of attenuation readable the scale was opened out by a series of gears free from back-lash and an 8" dial used for calibration.

One decibel variation at the lower end of the scale gave a dial movement from the pointer of 1/8", at the 20 dBs. position the movement opened out to $\frac{1}{2}"$, from then on the movement was substantially linear. By a double rotation of the dial a variation between 0 and 80 dBs. was obtained.

The method of calibrating the attenuator was simply to connect a standard signal generator to the feeder in place of the aerial and vary the generator output by the wanted amount and change the attenuator dial position to bring the receiver output back to a reference level. This calibration was cross-checked with the aid of a test signal injection box and dummy aerial.

The injection box was a very simple unit consisting of a caged portion of the inner conductor of the feeder into which the generator, terminated by a 75 ohm resistance, injected a test signal. This unit was very useful in adjusting and checking the aerial and also in checking the receiver sensitivity on the aircraft.

The diode 2nd detector of the receiver was used as a source of D.C. signal supply to a Cossor Cathode Ray Oscilloscope unit.

During the first test flight it was found that the screening of the receiver was still far from perfect. Further investigation in the laboratory showed that the metal frequency indicating dial of the receiver was responsible for most of the unwanted pick up, this was suppressed by inserting a specially designed spring washer between the dial and panel. Similar spring washers had to be fitted to most of the protruding spindles on the panel.

An appreciable amount of unwanted signal was introduced into the set by the power mains lead and the output lead to the oscilloscope. Suitable filters had to be inserted in each of these leads and the leads screened.

(b) Transmitter.

A standard CD/CHL pulse transmitter working on a frequency of 200 Mc/s. was installed at the A/M transmitting station at Stock four miles south of Chelmsford.

A 70 ft. wooden lattice tower was available on the site and a simple vertical dipole installed at the top of it. The aerial was carefully lined up and the usual checks made for standing waves on the 200 ohm balanced feeder connecting the transmitter fo the aerial.

The transmitter was capable of radiating about 25 kilowatts peak power.

During the first test flight a pulse width of 4 microseconds was used with a P.R.F. of 500. An interval signal was incorporated in the modulator for the purpose of identification.

From the results of the first flight it was considered that a gain of 15 dBs. was necessary to do the tests well. It was obviously impracticable to raise the transmitter power to this extent so it was decided to widen the transmitted pulse in order to give the S.27.CA receiver a better chance to accept it. The P.R.F. was reduced to 50 to conserve the power available to the transmitting valve anodes.

Extra capacities were banked on to the anode and grid pulse forming circuits and a new modulator was made; under these new conditions a pulse width of 15 microseconds was obtainable, this increased pulse width gave an effective 12 - 13 dBs. gain at the output of the receiver.

During the second test flight it was found that due to the great number of pulse stations working on or around 200 Mc/s. with P.R.F's between 150 and 400 the 50 P.R. F. was rather difficult to find although once the C. R.O. time base had been synchronised it was easy to hold. Therefore for the third test it was decided to increase the P.R.F. as far as possible without decreasing the power output of the transmitter. The receiver to be used on the test was set up 4 miles from the transmitter and the P.R.F. increased until the received signal strength commenced to decrease, this point occurred at a P.R.F. of 200 and this condition was used for the remaining four tests.

Installation of equipment on the aircraft.

192 Squadron, R.A.F. kindly allocated a Wellington aircraft for these tests.

Supplies for the receiver and C.R.O. were obtained from a rotary converter driven by the aircraft's floating accumulators. The output from the converter was 230 volts 50 cycle A.C.

The aerial used was a $\frac{1}{4}$ wave vertical rod with a 2 feet square brass plate at the bottom end; an insulator was inserted in the centre of the plate to support the aerial.

The brass plate was bolted on to the geodetic of the aircraft and located just aft of the astro-dome. Special attention was paid to bonding the equipment to the aircraft structure.

The equipment was installed immediately beneath the aerial. The aerial was adjusted and the sensitivity of the receiver checked before each flight by means of the injection box mentioned previously.

Special Meteorological Equipment.

After the first two flights it was decided that meteorological data taken during the flight was necessary, therefore an aneroid barometer and a psychrometer were borrowed from an R.A.F. Meteorological Station.

The aneroid barometer was mounted on a sprung base-board and installed inside the aircraft near the starboard waist window.

The psychrometer was installed outside the aircraft near the starboard waist window in such a way that the dry and wet bulbs of the thermometers could be read by an operator in the waist of the aircraft.

The position of the psychrometer in respect to the slip stream of the aircraft was fully discussed with the Meteorological Station and it was their opinion that the position was satisfactory.

Method of making signal measurements.

Several methods of making signal measurements were tried in the laboratory and the one finally adopted was the method of adjusting the attenuator so that the signal just came down to set noise. Readings of the order of \pm 0.5 dBs. could be repeated even with different operators. This method proved quite satisfactory in the air.

Before each flight the watches of the navigator and the special operator were synchronised. The special operator took readings each minute, and during some periods every half minute, throughout the flight and the data analysed afterwards with the aid of the navigators log.

The meteorological instruments were read at the appropriate heights. Reliability of measurements.

There is evidence to suggest that the measurements taken are remarkable reliable.

It will for instance be noted, upon reference to the data sheets, that during the flight of the 22/4/44 three straight runs were made at 10,000 ft, the average reading for each run was 28.5, 29.2, and 28.8 dBs. respectively. Each of these values was the average of five to six readings.

The worst divergence of individual readings from the average was less than \pm 2 dBs.

The averages of the three straight runs at 10,000 ft. on the 25/4/44 are equally good.

Only two straight runs at 10,000 ft. were made on the 20/4/44 and 23/4/44 but here again extremely close agreement exists.

Throughout each test the transmitter was monitored on a second receiver located on the ground four miles from the transmitter.

First Test Flight 27/1/44.

The first test flight was very much in the nature of trying out the equipment and the general conditions under which the tests were to be carried out and to find out what modifications to equipment, test conditions, and programme had to be made for future tests.

When the tests were planned it was considered possible to make the height gain tests over the 192 Squadron's airfield in Norfolk but upon investigating the ground contour along the signal path it was realised that a very high hill was directly in the signal path and only one mile from the transmitter.

The only free routes away from the transmitter were due east and west north west. The east route was ruled out owing to the proximity of enemy occupied territory. Accordingly the air-crew was briefed to fly from their base in Norfolk to Chelmsford to Buckingham at a constant height of 2,000 feet. At Buckingham the aircraft was to spiral up to 10,000 ft. and at that height to patrol between Bicester and Towcester on a steady compass bearing; the line joining these two places is at right angles to the line joining Chelmsford and Buckingham, therefore the aircraft was flying on an equidistant course from the transmitter. After the aircraft had completed the 10,000 ft. straight run it was to fly back to Bicester and run in again on the same patrol course at 9,000 ft. and maintain that height throughout that run.

After each patrol the aircraft was to descend 1,000 ft. until it reached 4,000 ft., it was then to descend in 500 feet stages down to 500 feet.

The attached track chart shows the route taken and the method of timing for correlating signal measurements.

During this test flight it was confirmed that the Norfolk - Chelmsford route was completely unsuitable for the tests planned and that the Chelmsford - Buckingham route was satisfactory.

The signal measurements between Chelmsford and Buckingham give a good idea of the attenuation along the route. Although this did not form part of the original programme it was included in each test as it was obviously of general interest.

. The Height-Gain measurements and the attenuation measurements have been tabulated on an appended sheet.

It will be seen that the measurements made during the spiral climb are very erratic, due without a doubt to the polar diagram of the aerial being affected by different positions of the aircraft in respect to the transmitter and by the tilting of the aerial while banking.

The step by step straight run Height-Gain measurements were quite reliable.

It is pointed out that the measurements for the 27/1/44 test have all been corrected by + 12 dBs. (the gain obtained by increasing the pulse width after the first test) in order that they may be readily compared with the remaining five tests.

All curves have been plotted on a linear scale and are shown on a separate sheet so that they may be compared easily one with the other. All distances and heights have been converted to kilometers and metres to facilitate the analysis of the data.

Second Test Flight 29/2/44.

Necessary modifications to the equipment were made between the first and second test flights. For the second flight it was considered necessary to make the Height-Gain measurements at a greater distance in order to make sure that the aircraft went well beyond the horizon; the patrol line was therefore in the Leamington area.

It is of great interest to note that the signal on this occasion could not be found above about 6,000 ft. during the spiral climb and was picked up again during the descent at about 7,000 ft.

The discrepancy between these two heights may be explained by the fact that the rate of climb was assumed to be constant whereas it probably fell off towards the higher levels; the level at which the signal dropped out was therefore probably nearer 7,000 ft. during the aseent.

The cut-off of the signal was extremely sharp as also was the reappearance on the descent. Although no measurements were possible it is almost certain that the signal went through this violent change in about 200 - 250 feet change in altitude.

Upon analysing the meteorological report for that day it was found that wide-spread temperature inversions occurred throughout most of the day in the region of 7,000 ft. An extract from the meteors logical report for this day is attached.

Test Flights 20/4/44, 22/4/44, 23/4/44, 25/4/44.

These four flights were made under the same conditions and on the same route and can therefore be reported upon collectively.

The P.R.F. had been raised from 50 to 200 for these tests in order to make the signal more easily readable amongst the numerous pulse stations on the same radio frequency.

The meteorological instruments mentioned previously were installed in the aircraft for these tests and readings were taken only as the straight run patrols during the step by step descent.

In order to save time on the flight it was thought possible to make each alternate height-gain straight run on the reciprocal compass bearing; in other words the 9,000, 7,000, 5,000 etc. feet runs were made on the reciprocal compass bearing to that on which the 10,000, 8,000, 6,000 etc. feet runs were made.

A check was made at 10,000 ft. on each flight to see if this was permissible; therefore two or three runs were made at 1,000 ft. flying in opposite directions and of course still at right angles to the line joining the patrol area and the transmitter.

On each occasion the method was perfectly satisfactory and extremely close agreement of readings was obtained as already stated.

A further modification to the programme of these tests was that when the signal was lost at the end of the attenuation run at 2,000 ft. the aircraft was to descend to 500 ft. to check whether signals could be picked up again at a lower altitude; no evidence was obtained that this was the case.

It will be noticed upon reference to the set of height-gain curves that a marked "ledge" occurs between 7,000 and 9,000 ft. on the 20th, 22nd and 23rd of April.

In all these tests it will be seen that the measurements made during the spiral climb are too erratic to be made use of.

Conclusion.

The Eckersley Group desire to express their gratitude for the whole-hearted cooperation and help of Wing Commander Willis D.S.O., D.F.C. formerly commanding 192 Squadron; Wing Commander Fernbank D.F.C. commanding 192 Squadron; Sq/Ldr. Mazdon and his Special Signals Section also of 192 Squadron; and the many Aircrews who carried out so well the very tedious flights.

Symbols used in report.

T = Time in B.S.T.

Kms. = Kilometres.

TX. = Transmitter.

Hm. = Height in metres.

Temp. = Temperature in degrees F.

Hum. = Humidity in %.

mbs. = Millibars.

Inclusions.

Six sheets of tabulated attenuation and height-gain readings.

One sheet of meteorological readings.

One sheet of attenuation and height gain curves.

One track chart.

One extract from the meteorlogical report 29/2/44.

	Atten	uation.		Height-Gain.					
т.	Kms. from TX.	dBs.	Hm.	T.	Kms. from TX.	dBs.	Hm.		
1327 1328 1329 1330 1331 1332 1333 1334 1335 1336	6.2 9.3 12.4 15.5 18.6 21.7 24.8 28.3 31.8	52 51 56 51 47 43 43 39 36 37	600	1356 1357 1358 1359 1400 1401 1402 1403 1404 1405	11 11 11 11 11 11	23 27 32 32 32 34 31 35 36 29	600 720 840 960 1080 1200 1320 1440 1560 1680	Spiral	
1337 1338 1339 1340 1341 1342 1343 1344 1345 1346	38.8 42.3 45.8 49.3 53.8 57.3 60.8 64.3 68.8 72.3 75.8	33 31 32 28 28 26 27 26 24 25 24	# # # # # # # # # # # # # # # # # # #	1406 1407 1408 1409 1410 1411 1412 1413 1414 1415 1416		34 40 44 41 42 44 36 32 31 29 25	1800 1920 2040 2160 2280 2400 2520 2640 2760 2880 3000		
1348 1349 1350	79•3 83•8 87•3	22 22 21	11	T1/	Kms.	Average. dBs.			
1351 1352 1353 1354	90.8 94.3 97.8 101.3	20 21 19 18	1) 11	1417 1423	114	32.4	3050		
1355	104.8	21	11	1435	Z II	32.3	2740		
				1450 1455	n ` -	33	2430		
				1506 1513	."	31.2	2120	Straight	
Parantzi				1523 1529		32	1820	Run	
				1539 1545		28.4	1520		
		PRODUCTO (I		1555 1602	" \	26.1	1220		
				1611 1617		24.3	1070		
• (1)		•		1627 1633	H ,	23.3	910		
. h -	•			1643 1649	n'	19	760		
				1650 1658	, n	18.5	600		

	Attenua	ation.		, , ,	Height-Wain.					
т.	Kms. from TX.	dBs.	Hm.	T.	Kms. from TX.	dBs.	Hm.			
1031	0	54	600	1105	148	10.	600	EF 61		
1032	4.65	51	11	1106	11)	- W	750			
1033	9.3	53	H	1107	II.	- Tree -	900			
1034	14.0	51	11	1108	11	16	1050			
1035	18.6	49	н	1109	11	N.R.	1200			
1036	23.2	48	11	1110	11	16	1350			
1037	27.9		11	1111	11	27	1500			
		45	110 11		tt.					
1038	32.6	45		1112		23	1650	Climb		
1039	37.2	43	"	1113	"	22	1800			
1040	41.8	42	"	1114	11	- 188	1950			
1041	46.6	41	ti	1115	11:	- 1	2100			
1042	50.6	38		1116	11	110-	2250			
1043	54.6	39	11	1117	11	- 26	2400			
1044	58.6	38	11	1118	11	100-	2550			
1045	62.6	33	11	1119	11	100 L	2700			
1046	67.4	35	11	1120	11	_	2850			
1047	72.2	33	"	1121	11		3000			
1048	77.0	29	11				,000			
1049	81.8	28	11	T1/	Kms.	Average				
	86.6		"		rom TX.		TIm			
1050		25		12. 1	. POII TA.	dBs.	Hm.			
1051	91.4	24	"	7707						
1052	96.2	22	"	1121	H					
1053	101.0	19	"	1127	148	-	3000			
1054	105.8	15	11	1135						
1055	110.6	15	11	1140	11		2700			
1056	114.3	14	11	7740	0.01		2100			
1057	118.0	15	11	1148				Straight		
1058	121.7	10	- 11	1153	11	-	2400			
1059	125.4	10	11							
1100	132.8	7	- 11	1154				Run		
1102	136.5	_	"	1200	11.7	25	2250	Av.H.		
1103	140.2		"	1201						
			11	1207	11	19	2100			
1104	143.9	•	"			+7	2,100			
1105	147.6	-	"	1214				,		
				1218	11	17.6	1800			
	•			1228						
				1233	11 10	15	1500			
				1234						
				1242	H **	12.5	1350	Av.H.		
					4	12.)	1))0	TA .TT.		
				1243						
			11	1247	11	-	1200			
				1255			7050			
			-0	1300	11	-	1050			
,		1		1309						
				1312	11		900			
			- 1				900			
			1	1321						
				1326	11	_	750			

	Attenua	tion.		Height-Gain.					
T.	Kms. from TX.	dBs.	Hm.	T.	Kms. from TX.	dBs.	Hm.		
1230	2	68	600	1314	177	_	150		
1231	6	41	11	1315	ii ii	-	270		
1232	10.2	49		1316	11	-	390		
1233	14.4	47	11	1317	00 H &	-	510		
1234	18.4	39	11	1318		_	. 630		
1235	22.4	37	11	1319	11	_	750	Spiral	
1236	26.5	37	11.7	1320	, н	10	870	Spiral	
1237	30.6	36	11	1321	g H 93	11	990		
1238	34.7	36	11	1322	. 11	14	1110		
1239	38.7	34	11	1323		11		Climb	
1240	42.7	32	11	1324	11	23	1350	axor	
1241	46.8	30	11	1325	11	14	1470		
1242	50.9	28	11	1326	n n	15	1590		
1243	55.0	27	11	1327	n	15	1710		
1244	59.1	28	11	1328	11	19	1830		
1245			11	1329	n n	22	1950		
	63.1	26	11	1330	, n	14	2070		
1246	67.2	24		1331				The A	
1247	71.2	24			11	15	2190		
1248	75.3	22	"	1332	11	16	2310		
1249	79.4	15	11	1333	17 11	16	2430		
L250	83.5	17	11	1334		14	2550		
1251	87.6	17		1335		13	2670		
1252	91.6	15	11	1336	"	15	2790		
1253	95.7	15		1337	"	11	2910		
1254	99.8	12	- 11	1338		14	3000		
255	103.9	, 10	11	/					
1256	108.0	7	"	T1/	Kms.	Average			
258	112.0		н	T2.	from TX.	dBs.	Hm.		
259	116.0	-	150						
1300	120.1		11	1339					
1301	124.2	_	. 11	1344	177	20	3000		
1302	128.3	_	. #	1345					
1303	132.4	-	11	1351	* n	19	3000		
304	136.5		- 11	1771		1))000	- 30L)	
1305	140.6	_	11	1352					
1306	144.7	- E-	11	1359	11	16.8	2740	Straight	
1307	148.8		- 11	1400				a agus.	
1308	152.9	_	11	1406	- 11	17	0470		
309	. 157.0	_	- 11	1400		17	2430	Run	
.310	161.0	_	11	1407				nun	
311	165.0		11	1413		12.5	2130		
312	169.0		11						
1313	173.0		н.,	1414					
314	177.0	0.0	11	1418	ıı .	11	1830		
-) 17	111.0			1419					
		HI .	. 4	1427	11		1530		
				1			1))0		
				1428					
				1433		-	1220		
				1434	* -				
					, ,		1070		
				1440		•	1070		
				1441					
				1447	11		920		
							,		
				1448					
			1				7/0		
				1453	. "		760		
				1453	. "		760		
		•		1453 1454		-			
			,	1453	п .	-	600		
				1453 1454		-			
				1453 1454 1500 1501		-	600		
			,	1453 1454 1500 1501 1508	11	-			
				1453 1454 1500 1501 1508 1509	11	-	600 460		
				1453 1454 1500 1501 1508	11		600		
				1453 1454 1500 1501 1508 1509	11		600 460		

	Attenuat	cion.		Height-Gain.						
т.	Kms. from TX.	dBs.	Hm.	T.	Kms. from TX.	dBs.	Hm.			
1300	4.8	53	600	1338	154		150			
1301	6.4	56	11	1339		-	290			
1302	. 9.6	49	fi e	1340	r e e		435			
1303	12.8	54	11	1341		-	585			
1304	16.0	47	- 11	1342	"	70	720 865			
1305	19.2	41		1343 1343 2	11	10 18	930			
1306	24.6	41	11	1344		15	1000	Spriral		
1307	28.7	38	"	13441	11	15	1020			
1308	32.8	38	11 41	1345	11	17	1150			
1309	36.9 40.1	37 32	- 11	1345=	. 11	21	1200	Climb		
1311	44.2	30	- 11	1346	11	17	1290			
1312	49.3	27	11	13461	11	22	1350			
1313	53.4	28	7 H 1	1347	11	24	1460			
1314	57.4	27		1347불	11	23	1500			
1315	61.5	23	. 11	1348	"	- 21	1570			
1316	65.6	19	11	1348	H	24	1650			
1317	69.7	21	n H	1349	"	25	1730			
1318	73.8	16	11	134%	."	23	1780			
1319	77.9	15	" "	1350		25	1850			
1320	82.0	13		1351 *	11	26 22	2140			
1321	86.1	13	11	1352 1353	ti ti	23	2280			
1322	90.2	12	11	1354	11	20	2430			
1323	94.3 98.4	10	11	1355	it.	24	2570			
1325	102.5	. 6	, 11	1356	H	23	2720			
1326	106.6	6	11 .	1357	H .	30	2850			
1327	110.7	-	11	1358	H	22	3000			
1328 1329 1330	114.8 118.9 123.0	-	11 11	T1/ T2.	Kms. from TX.	Average dBs.	Hm.			
1331 1332	127.1 131.2		11	1359						
1333	135.3		150	1401	154	28.5	3050			
1334	139.1 142.9		"	1402	11. E	29.2	3050			
1336	146.7	-	11	-		27.2	,0,0			
1337 1338	150.5 154.3	1.5	11	1407	. 11	28.8	3050			
1))0	1)4.7			1413						
				1420	it .	22	2740	Straigh		
				1421	11	22	2430	Run		
				1428		22	2430	Ituli		
				1429 1436		22	2130			
								\		
				1437	. 11	17	1830			
						-1	10,0			
				1445	11	13	1530			
						1)	1),0			
				1453	54		7000			
				1/150	11	1-4	1//11			
				1458	(7.5	1220			
				1459		7.5				
			• = = 4	1459 1507	"	-	. 920			
			•	1459 1507 1508	H .	7.5 -	. 920			
	908 1008			1459 1507 1508 1514		7.5 -				
	008 008 791			1459 1507 1508 1514 1515	" "	7.5 - -	. 920			
	000 600 731			1459 1507 1508 1514 1515 1521	H .	7.5 - -	. 920			
	908			1459 1507 1508 1514 1515	" "	7.5 - -	. 920			

	Attenua	tion.		Height-Gain.					
T.	Kms. from TX.	dBs.	Hm.	T.	Kms. from TX.	dBs.	Hm.		
1200	2	EA		1234	147				
1200		54	600	1235	14/	-	150 420		
		61		1235=	H				
202		53	11		L n	•	540		
L203	14.9	49	11	1236		-	660		
1204		47	#	12362	11	•	780	Spiral	
205	23.5	45	11	1237	11	-	900		
206	27.8	42	11	1237를	11	12	1040		
207	32.1	38	n.	1238	- 11	15	1140		
1208	36.4	40	11	1238 2	11	16	1260	Climb	
209	40.7		11	1239	A n	15	1380	CITHO	
		39	11	1239	11				
210	시하는 사이트, 현존 시간에서 양성하는 시에 들었다는 게 되었다.	37			11	15	1500		
211	49.3	35	".	1240		18	1620		
212	53.6	32		1240불	- 11	22	1740		
1213	57.9	33	11	1241	11	16	1860		
214	62.2	30	11	1241=	11	19	1980		
215	66.5	28	11	1242	н	26	2100		
216	70.8	26	11	1242=	n I.	26	2200		
.217			11	1243	H H	21	2340	A ST	
	75.1	27			11				
218	79.4	24		1243 2		29	2460		
.219	83.7	23	tt .	1244	"	31	2580		
.220	88.0	21	11	12442	11	28	2700		
221	92.3	19	11	1245	11	31	2820		
222	96.6	19	11	1245		26	2940		
223	100.8	16	11	1246	11	22	3050		
.224 .225 .226	105.1 108.4 112.7	15 15 12	" II	T1/ T2.	Kms. from TX.	Average dBs.	Hm.	922122 12082	
227	117.0	11 7	. "	1250				4.801	
.229	125.6 129.9	-	150	1254	147	29.6	3050		
L231 L232	134.2 138.5	7.0	11 11	1300	u per	29.5	3050		
1233	142.8 147.1	- -	11 - 12	1301	. n	24.5	2740	Straight	
		, Sant		1308 1313	н ,	.24.6	2430		
				1314 1318	. in	24.0	2130	Run	
			j.	1319 1325	ž 11	22.5	1830		
				1326 1332	11	16	1530		
			ſ	1333 1338	ı, ıı	14.5	1220		
	385			1340 1345	H ,	5	920		
	091	(6	1346 1349	e n	-	600		
				1350 1355	n · ·	-	300		
	(00)			1356 1400	T II	-	150		
			e de la companya de l	100000					

	Attenuation.				Hei	ight-Gain.		
т.	Kms. from TX.	dBs.	Hm.	T.	Kms. from TX.	dBs,	Hm.	2 13 135
				1632	140		150	
1559	4.75	64	600	1633	140		400	
1600	9.5	50	"	1634	11		650	
1601	14.2	61			11			Spiral
1602	19.0	46	11	1635		i line	900	
1603	23.8	47	11	1636	U	7	1140	
1604	28.5	45	II	1636=	"	10	1260	
1605	33.2	42	11	1637		11	1400	
1606	38.0	41	11	1637章	и	13	1530	
1607	42.7	42	11	1638	11	14	1650	Climb
1608	47.5	36	. 11	16382	11	12	1760	
			11	1639	11	15	1900	
1609	-52.2	37			H		2010	
1610	57.0	32	"	16392		15		
1611	61.8	26	"	1640	U	20	2140	
1612	66.5	23	- 11	16402	11	15	2260	
1613	71.2	25	- 11	1641	- 11	19	2400	
1614	76.0	25	11	1641	n	15	2500	
1615	79.4	19	11	1642	11	21	2640	
1019			- 11	16421	11	20	2700	
1616	82.9	21			- 11			
1617	86.3	19	. 11	1643		23	2890	
1618 1619	89.8 93.3	18 16	11	1643호	"	,22	3050	
1620 1621	96.7 100.2	11 10	t) 	T1/ T2.	Kms. from TX.	Average dBs.	Hm.	
1622 1623 1624	103.6 107.1 110.6	9	"	1644 1648	140	24.8	3050	A COSS
1625 1626 1627	114.0 117.5 121.2	6 - -	150	1649 1657	11	24.3	3050	18.09 18.00 0.1
1628 1629 1630	124.9 128.6 132.3		"	1658 1702	. 11	25.4	3050	Straigh
1631 1632	136.0 139.7		n n.	1703 1712	was n	22.3	2740	Run
				1713 1718	ıı ı	18.0	2430	
				1719 1725	. 11	16.0	2130	
			1875	1726 1733	ıı	13.5	1830	
				1734 1740	» II	11.5	1530	
				1741 1746	п	-	1220	
				1747 1753	(1) (1) (1) (1) (1)	-	920	ere of
			hiliketiji. Edinomini	1754 1759	11		600	
			,	1800 1807	h.	-	300	
				1808 1815			150	
				1816 1822	ıı,	_	150	

GAI/JOB.

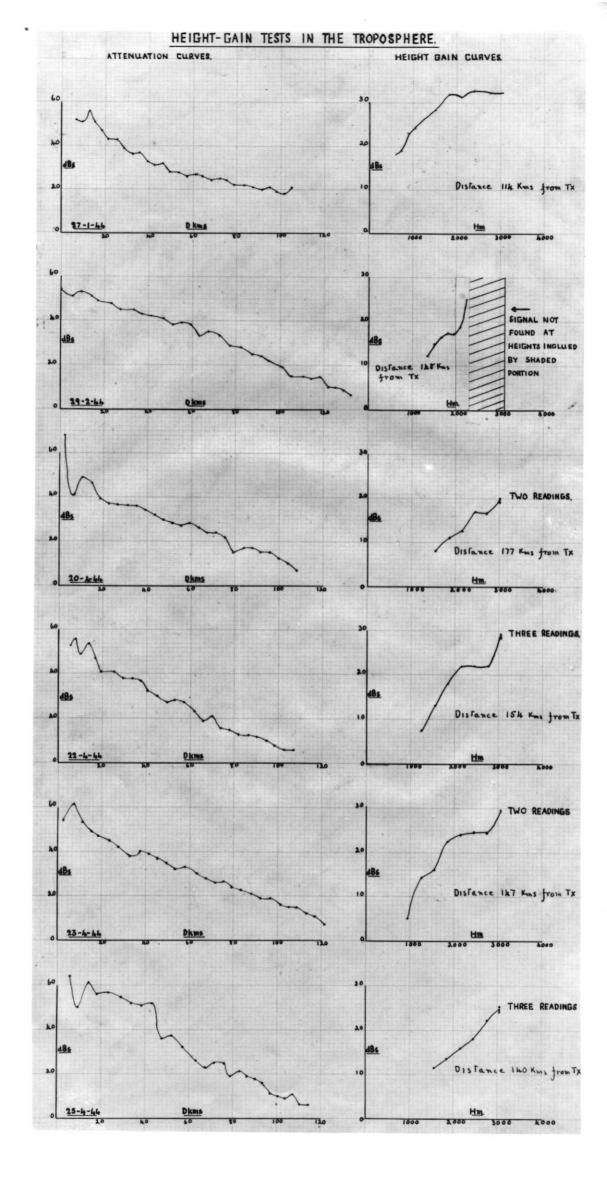
Height-Gain Tests in the Troposphere.

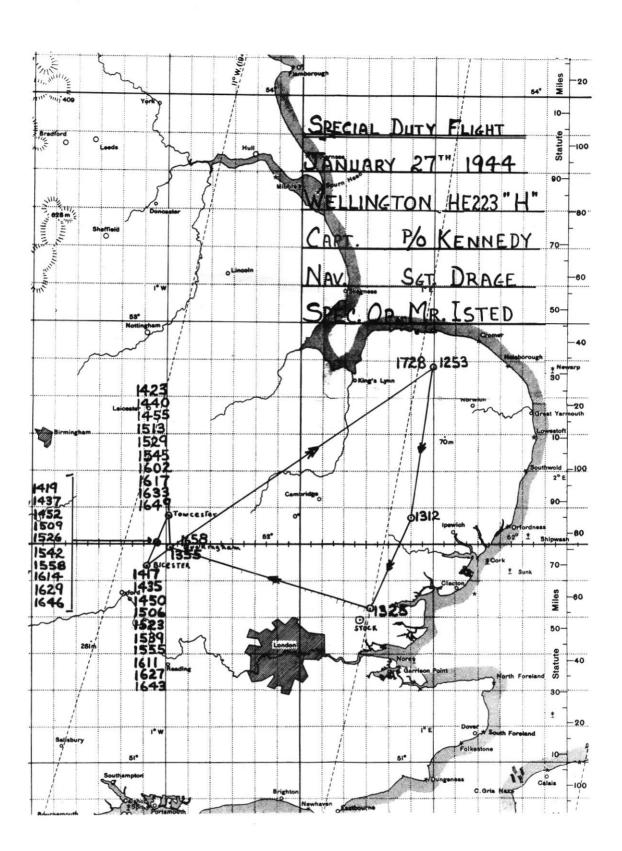
Meteorological Data.

		44.	29/2/4					27/1/44.		
	T.	Pres.	Hum.	Temp.	Hm.	.T.	Pres.	Hum.	Temp.	Hm.
	1300	677	40	6	3050	1500	700 mbs.	64%	27°F.	3050
	11	705	44	8	2740	11	727	60	29	2740
	11	734	53	9	2430	11	756	56	32	2430.
	11	764	58	11	2130	11	785	55	33	2130
Spiral	11	795	59	14	1830	11	815	58	37	1830
phriar	11	827	63	16	1530	11	846	70	37	1530
	- 11	860	67		1220	11	879	74	41	1220
	11		68	19	920	11	913	77	45	920
	11	894		23		11		11	48	600
	11	929	70	28	600	11	947	81		
Climb		964	69	33	300		992	81	47	300
	11_	-	-	-	150	"		-	344	150
		14.	22/4/4				.1		20/4/	
	T.	Pres.	Hum.	Temp.	Hm.	T.	Pres.	Hum.	Temp.	Hm.
	1450	706	88	29	3050	1430	694	46	21	3050
		7	-	-	2740	"	724	53	23	2740
	, n	762	15	35	2430	11	752	60	25	2430
	11	792	15	37	2130	"	782	66	26	2130
	11	824	19	38	1830	11	813	71	28	1830
	11	855	57	42	1530	11	845	76	30	1530
	11	888	39	45	1220	***	878	76	34	1220
	11	916	30	49	920	11	913	74	39	920
	11	956	59	51	600	11	946	71	45	600
	tt .	990	82	57	, 300	.11	967	69	47	300
	11	1002	-	59	150	11,	-	-	-	150
- ,		14	25/4/4					'ΔΔ	23/4/	
	T.	Pres.	Hum.	Temp.	Hm.	T.	Pres.	Hum.	Temp.	Hm.
1	1730	688	64	25	3050	1330	705	55	31	3050
	11	724	63	26	2740	11	730	57	33	2740
	11	755	62	27	2430	11	758	42	36	2430
	- 11	788	60	28	2130	11	783	57 .	37	2130
	11	809	60	32	1830	,11	815	73	41	1830
	11	848	65	34.5	1530	11	848	84	44	1530
	11				1220	11				1220
		873	65	37		11	878	73.	47	
Straigh	"	910	66	40	920	"	906	93	44	920
	"	944	64	45.5	600		937	85	48	600
		977	62	50.5	300	"	-	-	-	300
	11	996	61	53	150	11	-	-	-	150

Note:- The data for the 27/1/44 and 29/2/44 was supplied by the Meteorological Office.

The data for the 20/4/44, 22/4/44, 23/4/44 and the 25/4/44 was obtained from meteorological instruments on the aircraft.





	LARKHILL	LARKHILL	LARKHILL	DIO-SOUNDING	LIVERPOOL	LIVERPOOL	LIVERPOOL	LIVERPOOL	DOWNHAM MARKET DOWNHAM MARKE
Processre M.S.L.	G.N.T.	0600 G.M.T.	1,200 G.M.T.	1800 G.M.T.	0000 G.M.T. 1004-2 mb	0600 G.M.T. 1002-2 mb	logi-2 hb	1800 G.M.T 959-2 ml	1001-5 mb 1000-5 m
Surf. Proceing	Surface mb	Sunface mb	988 mb	968 mb	Succes mb	Suctace mb	909 mb	900 mi	960 mb Surface m
Prosecure	Ball of Min Dir. Vel.	Dir. Vel. 1	Wind.	Dir. Vet.	Wind.	2 op % knots	E E Dir. Vel.	Dir. Vel	The property of the property o
Surf. 1000 950	0-5	04 423 28 360 6 0-8 14-1 27 26 360 21 8	04 37 73 330 10	04 34 80 270 6	00-050 83 Calm	00 627 86 Calm	03 68 230 A 13-934 70 250 16 C	00 ·640 86 260 10 0-2 3-4-57 88 280 214	01.256 83 Calm 01.28 92 Calm 0.4 0.1 85 50 18 6 13-3 28 97 90 10
800	27-7 21 36 40 21 42-3 16 73 40 22	280 21 88 m 18 M 425 15 86 20 12 A 57-8 9 54 20 19	284 23 23 230 15 13 2 17 70 250 15	18-6-26-25-300-18 13-3-20-00-00-16	8-4 22 60 560 II 4 48-0 15 67 350 II	27-3 26 76 260 17 42-5 17 31 230 15 57-8 19 20 330 166	28-0,5043 P7- 16-142-8 22-26 28-16-6	27782 20 286 24 426 26 24 286 24 56:1 21 26 226 25	1378 34 64 50 19 11 273 23 89 50 13 123 17 88 40 19 141 9 17 102 20 15 1578 11 86 20 21 572 10 109 10 15
750				75 1 12 DO 360 21			1 1 1 1	24-7 21 50 300 26	139 6 2 10 20 73:3 3 87 860 12
650	90-6-4-43 20 21 109-6-61 20 31 - 128-9-38 30 41	128 2 27 20 40	1110 3 43 20 27	111 16 50060261	813 50040 8 00 3 74 860.22 28 1 66 10 27 50 8 87 20 33	739 3, 86 360 21 310 8 70 360 22 00 3 70 360 24 129 2 71 360 30	INDICATE DEDAO 45 H	111 9 83 310.78	109 19 16 30 19 108 14 30 30 18
500	171 2051 50 57	172 17 49 20 36		73 43 83 10 30			75 17 70 550 2	175 16 100 510 28	171 16 29 50 57R 171 17 56 50 58
400	196 25 56 30 63 223 40 37 30 64 262 53 - 30 61	137 26 51 20 57	225 36 100 20 32 8	1224 H2 \$6030		773 15 86 36-36 197 27 91 36-36 234 33 83 10 36 264 31 - 10 32	25 28 75 260 20 6 224 40 80 260 28 266 63 350 254	224 42 - 300 27	23 38 33 30 50 223 41 - 30 60 253 50 40 60 1 252 53 . 20 53
300 250				286 67 0 28	287 66 20 47	826 -81 - 360 27	288 67 360 21 326 79 360 24	(380-4)	286 62 40 60 285 67 30 42 324 72 300 55 323 77 50 42
.,0		65 860.28	57.2 72 See 27 560.25	- 171 - 51034	- 25 54017	72 - 520-26	72 330 276		570 75 - 80 33 568 73 - 360 24 - 77 - 10 21 - 68
130	73 36 30	432 46 - 840 21 - - 66 - 810 17 - 68 - 320 28	432 67 360 226 68 340 25 70 310 24	- 77- 22033	75 3020	428 % · 510 27 c - 24 · 510 34 - 77 · 800 38	431 76 326 25 A - 72 310 26 - 63 28031		129 70 - 360 20 1 - (3) 10 18 - 71 - 360 22
80 90	513 60 · 340 25 68 · 520 20 71 · 310 15		517 68 280.27 67 280.29 69 270.40	510 73 - 280-47 73 - 280-42 73 - 270-43 75 - 270-45 75 - 240-40	77 250-28 78 810-32	511 77 · 250 33 76 · 280 35 73 · 280 31	514 70 28030 71 28045 40 28042		73 - 35024 73 - 36021 75 - 840 16
70 60	49 29029		67 290 35	75 276.45 15 260.40	77 0032 73 3032	lartraion:	64 28042 70.34	nversion.	76 - 040 17 73 - 030 22 130 Hermal:
	700mb -4° to	986mb 23° to 960mb 23°	lisothermall: 750-700mb 6°	988mb 34° to 970mb 35°	980 mb 32° to	970 mb 31°	riomb 10° to seems 13° bothermal:	romb 20° to roomb 21° sothermel:	500-430mb - Ko 750mb 3° bo
		700mb -20to 670mb 10 630mb -30 to		750 mb 13° to	720mb -2° to 700mb 1°	720 mb 10°	10-Soomb 219	700-770mb 20°	premier: promise so to contract of the contra
Tropo-	Type I 250mb -76°	Type I 260mb - 24°	Type \$ 240mb -80°	800-730mb 18° MPC I 246mb -83°	Type II 250mb-86°	Type I 220mb-87	Repe 1 230mb -82°	Note	33,000ft. 3,500fc.
	DOWNHAM MARKET	DOWNHAM MARKET	LERWICK	LERWICK	LERWICK	AS 200 ft. LERWICK	PENZANCE PENZAN	CE PENZANCE PEN	BANCE VALENTIA VALENTIA LEVONAMI
M.S.L. Suri,	1200 G.M.T. MOOI S mb	1800 G.M.T. 1000-5 mb	987-2 mb	0600 G.M.T. 983-2 mb 973 mb	784.2 mb	988-2 mb	1001 mbroog	mb 1005.7 mb 1005	mb 1007 mb 1003 mb 333 c m
Pressure sub	Thouse The state of the state o	Wind.	#8 Wind. Dir. Vel. T	# 5 E Wind. T	AS E Wind. Dir. Vel. T	Wind. T	Height Hum was	8 -0 6 8 -0	Hum
Surf			02:237 00 22-30	02 17 40 80 26020	P3 .7 37 72 300 IS	描" 字 % kneta	Z	% I 90 I	4 % 2
950 900	13.8 27 61 310 7 9	13-6 32 60 270 14 6	034	00441 75 260308	093 3478 310 18 B	6-2 50 69 810 15 B	14-4-190 73 14-6 128 7 28-4-194 76 198-6 123	10 15 · 1 36 60 4· 6	25 00 237 27 23 20 05 87 13 423 - 12 00 237 27 23 20 05 88 27 3 20 - 12 00 446 21 81 438 30 31 423 25 -
800.	423 15 34 320 10 -	42.421 83.300 20 58-0 20 78340 13	549 22 98 250 42 ·	54-120 78 280-44	13-6 15 24 300 28	54212	58-3 10 88 58-4 9	2 503 II DI 533	00000 4 86 597 26 89 570 20
750 700 650	73-7 8 23340 8- 50-8 4 21360 M	74-3 12 84 350 10 · 81-6 11 64 340 26 ·	71.4 18 75 26034 - 18.9 14 66 270 83 - 19.53 270 33	703 14 77 270 46 879 12 56 260 44 106 5 83 260 43	3-9 10 87280 48 3-70 3 51 260 63 103 4 86 260 60	73095260358 05-700260-3	74.4 4 64.746 7 6 61.6 5 81 81.6 6 6 110 2 80 110 5	\$ 75.6 16 86 75.6 15 83.0 1	2 00 762 16 51 764 26 16 743 15 - 16 57 537 15 65 54 2 20 32 51 7 14 - 0 54 112 5 41 113 13 41 110 5 - 2 50 132 5 24 133 .5 44 130 3 .
	150 -9 39 20 28	151 8 6836023	10 3 3 280 28	147-8-5270-48	146 -8 23 270 77	145 21 00 200 56	151 7 77 151 8	6 153 5 63 153	6 85 153 -4 25 154 -4 40 151 5
450	187-2763 10 26-	198 20 79 550 24-	97 24 57 28 30-	176 17 5427648 184 27 5427648 221 39 72 276648	220240 270 85	81 29 K5 R76 83	23537 78 225 35	33 227 35 74 227	1792 177 12 23 177 14 51 174 15 - 28 100 20 22 21 202 26 54 139 25 - 12 - 228 35 35 229 35 36 226 38 -
350	253-52 20 35	254-64 35024	253-45- 250-41-	251 55 - 276 67-	249 -51 276 776	-8-51 - 260 103D	288 64 - 288 63	20/ 40	4 291 62 - 291 64 - 29 - 4
250	323-8 10'32 .	376 -78 340 29 6	325 73 - 280-47 - 370 87 - 280-33 E	365-84 - 27666 - 3	126 70 260 81 166 77 260 8	9-71 - 27085	326 77 · 326 77 · 371 · 80 · 65 · 77 ·	828 74 - 827	291 62 - 281 66 - 287 64 - 277 829 -76 - 829 -76 - 829 -77 829 -77 829 -77 871 - 81 871 - 81
	428-71 300 178	429-72 309.22	127-83 - 280 25	422 84 - 27081-	24 77	28 73 - 75 61 6	431 43 430 71	433 63 431	
110	76 300 23 511 72 300 18		81 290.25 81 250.38 00 78 280.47	- 87 · 270.40 -89 · 260.46 -82 · 260.54	-8.3 27.43 -8.0 27.0 33 -2.0 27.0 35	75	514 71 514 73	518-66 - 514	
70	70 28023 -73 26033 -71 26034	76 29640	76 - 280 SI 78 - 200 SI		2 270 25 170 40 200 40 200 40 200 40	78 - 75 - 80 -		nversion: nvers 770mb 9 be open 760mb 16° Dooms	No humidin
~	770 mb 70 bo	hversion: 820mb 18° Eb		Somb 41°	30mb 6 60	Inversion: 978mb 30° to 970mb 32°	hversion: loothern somb lote 1002-100 bomb 50 350	al 620 mb 8° 840 mb a sothernal soon 760-740mb 1005	Inversion: Inversion: Surface
	(30 NO U			bothermal:	, ,	70mb .22 6	So form h wersion:	. 1003-1000#643	50 750mb 16 780mb 200
		Nomb 10° to		250-340mb 41° 730-700 mb 12°	į.	540mb-20° 520mb-25° bo 510mb-22°	10 470 170	/362/	bomb bothermali 0 750-740mb

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